

## Supporting Information

### Selective $\text{Fe}^{2+}$ Ion Recognition Using a Fluorescent Pyridinyl-benzoimidazole-derived Ionophore

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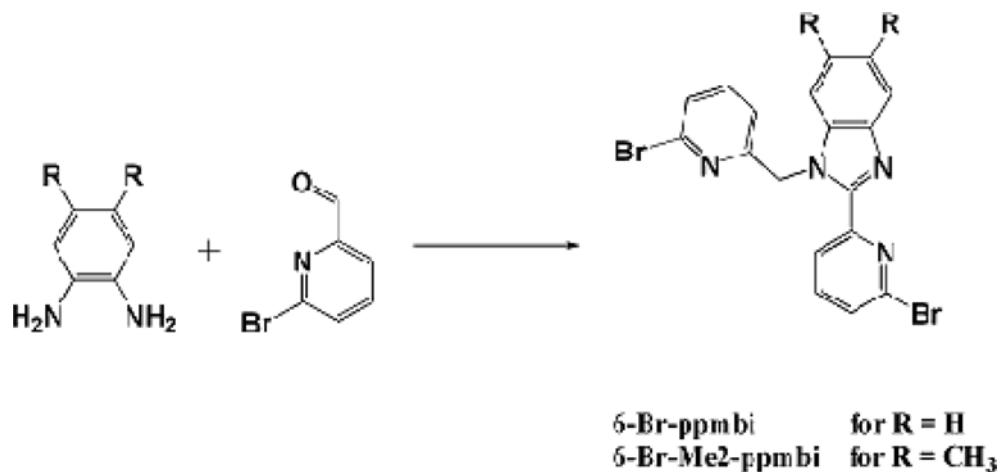
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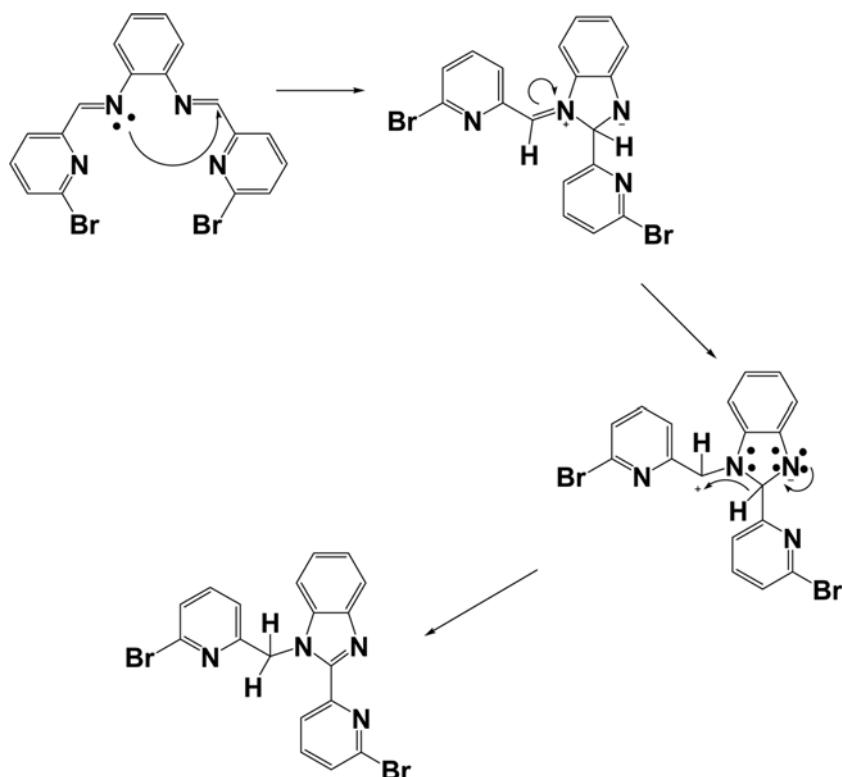
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Scheme 1

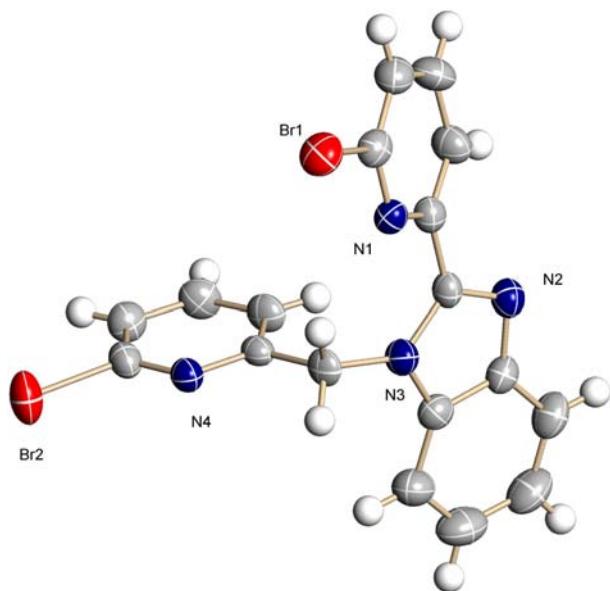


Scheme 2

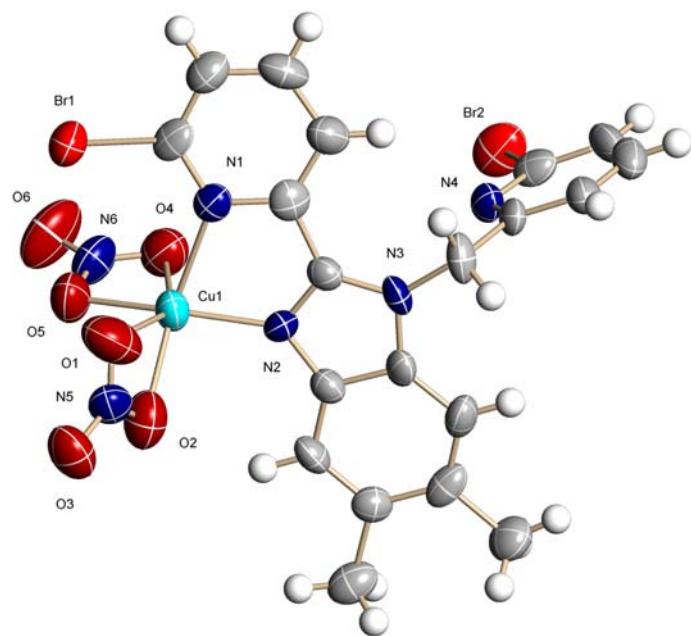
**Table S1.** Summary of X-ray Crystallographic Data for **6Br-ppmbi** and **[Cu(6Br-Me2-ppmbi)(NO<sub>3</sub>)<sub>2</sub>]**

	<b>6Br-ppmbi</b>	<b>[Cu(6Br-Me2-ppmbi)(NO<sub>3</sub>)<sub>2</sub>]</b>
Empirical formula	C <sub>18</sub> H <sub>12</sub> Br <sub>2</sub> N <sub>4</sub>	C <sub>20</sub> H <sub>16</sub> Br <sub>2</sub> N <sub>6</sub> CuO <sub>6</sub>
Formula weight	444.14	659.75
Space group	P <bar{1}< bar=""></bar{1}<>	C2/c
a, Å	8.0316(8)	11.4709(8)
b, Å	9.4623(9)	14.0339(8)
c, Å	12.0952(11)	15.5854(10)
α, deg	71.450(3)	104.777(4)
β, deg	85.303(3)	90.997(3)
γ, deg	77.525(3)	107.114(3)
V, Å <sup>3</sup>	841.83(14)	2306.9(3)
Z	2	4
Density (calculated), g/cm <sup>3</sup>	1.752	1.900
T, K	300	296(2)
Absorption coefficient, mm <sup>-1</sup>	4.821	4.462
Total no. of data	12544	26244
No. of unique data points	3911	8386
No. of parameters	217	635
R1 (%) <sup>a</sup>	4.78	7.62
wR2 (%) <sup>b</sup>	15.47	20.79
Largest diff. peak and hole, e.Å <sup>-3</sup>	0.504 and -0.893	0.817 and -0.555

<sup>a</sup> R1 =  $\sum ||F_0| - |F_c|| / \sum |F_0|$ .   <sup>b</sup> wR2 = { $\sum [w(F_0^2 - F_c^2)^2] / \sum [w(F_0^2)^2]$ }<sup>1/2</sup>



**Fig. S1.** ORTEP drawing of **6Br-ppmbi**, showing 50% probability thermal ellipsoids. It represents a highly hindered metal binding site composed with 6-bromo pyridine and imidazole motif



**Fig. S2.** ORTEP drawing of  $[Cu(6\text{-Br-Me}_2\text{-ppmbi})(NO_3)_2]$ , showing 50% probability thermal ellipsoids.

data\_ [Cu(6-Br-Me2-ppmbi)(NO<sub>3</sub>)<sub>2</sub>]

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?

;

\_chemical\_name\_common ?

\_chemical\_melting\_point ?

\_chemical\_formula\_moiety ?

\_chemical\_formula\_sum

'C20 H16 Br2 Cu N6 O6'

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loop\_

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\_atom\_type\_description

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'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'

'N' 'N' 0.0061 0.0033

'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'

'O' 'O' 0.0106 0.0060

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'Cu' 'Cu' 0.3201 1.2651

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'Br' 'Br' -0.2901 2.4595

'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'

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\_symmetry\_space\_group\_name\_H-M P-1

loop\_

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'x, y, z'

'-x, -y, -z'

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\_cell\_length\_c 15.5854(10)

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\_cell\_angle\_beta 90.997(3)

\_cell\_angle\_gamma 107.114(3)

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Refinement of  $F^2$  against ALL reflections. The weighted R-factor wR and goodness of fit S are based on  $F^2$ , conventional R-factors R are based on F, with F set to zero for negative  $F^2$ . The threshold expression of  $F^2 > 2\text{sigma}(F^2)$  is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-factors based on  $F^2$  are statistically about twice as large as those based on F, and R-factors based on ALL data will be even larger.

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C28 C 0.5466(11) 0.5708(10) 0.1161(7) 0.042(3) Uani 1 1 d . . .  
C21 C 0.1942(13) 0.1741(11) 0.1028(8) 0.055(4) Uani 1 1 d . . .  
C6 C 0.4035(12) 0.0485(9) 0.3706(8) 0.042(3) Uani 1 1 d . . .  
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C1 C 0.1323(12) 0.1213(11) 0.3328(8) 0.050(3) Uani 1 1 d . . .  
C5 C 0.3314(13) 0.1174(11) 0.3588(8) 0.052(3) Uani 1 1 d . . .  
C9 C 0.6521(12) -0.0430(12) 0.4074(8) 0.056(4) Uani 1 1 d . . .  
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 C12 C 0.4251(12) -0.2001(9) 0.3511(8) 0.048(3) Uani 1 1 d . . .  
 H12 H 0.3499 -0.2517 0.3339 0.057 Uiso 1 1 calc R . . .  
 C35 C 0.6587(11) 0.4404(10) 0.1125(8) 0.049(3) Uani 1 1 d . . .  
 H35A H 0.7099 0.4679 0.0700 0.059 Uiso 1 1 calc R . . .  
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 C19 C 0.8498(13) 0.2749(11) 0.2436(12) 0.064(4) Uani 1 1 d . . .  
 H19 H 0.9002 0.2961 0.2015 0.077 Uiso 1 1 calc R . . .  
 C11 C 0.5313(13) -0.2247(10) 0.3660(8) 0.048(3) Uani 1 1 d . . .  
 C26 C 0.4273(12) 0.4140(9) 0.1186(8) 0.043(3) Uani 1 1 d . . .  
 C37 C 0.8491(12) 0.5410(10) 0.2197(10) 0.057(4) Uani 1 1 d . . .  
 H37 H 0.8923 0.5530 0.1716 0.068 Uiso 1 1 calc R . . .  
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 C22 C 0.2537(16) 0.1059(11) 0.1177(10) 0.068(4) Uani 1 1 d . . .  
 H22 H 0.2098 0.0377 0.1146 0.081 Uiso 1 1 calc R . . .  
 C34 C 0.7057(13) 0.8489(11) 0.1269(10) 0.071(4) Uani 1 1 d . . .  
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 C20 C 0.7393(13) 0.1931(11) 0.2201(8) 0.054(4) Uani 1 1 d . . .  
 C33 C 0.4484(14) 0.8436(11) 0.1223(9) 0.065(4) Uani 1 1 d . . .  
 H33A H 0.3628 0.8307 0.1299 0.098 Uiso 1 1 calc R . . .  
 H33B H 0.4647 0.8625 0.0677 0.098 Uiso 1 1 calc R . . .  
 H33C H 0.4959 0.8991 0.1715 0.098 Uiso 1 1 calc R . . .  
 C13 C 0.5176(14) -0.3394(11) 0.3570(9) 0.066(4) Uani 1 1 d . . .  
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 C3 C 0.2945(16) 0.2733(11) 0.3508(9) 0.062(4) Uani 1 1 d . . .  
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 C17 C 0.8039(12) 0.2891(10) 0.3934(10) 0.055(4) Uani 1 1 d . . .  
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 C23 C 0.3784(17) 0.1413(12) 0.1370(11) 0.077(5) Uani 1 1 d . . .  
 H23 H 0.4207 0.0978 0.1483 0.092 Uiso 1 1 calc R . . .  
 C24 C 0.4401(14) 0.2426(11) 0.1393(9) 0.063(4) Uani 1 1 d . . .  
 H24 H 0.5245 0.2688 0.1541 0.076 Uiso 1 1 calc R . . .  
 C14 C 0.7585(13) -0.1734(12) 0.4095(10) 0.068(4) Uani 1 1 d . . .  
 H14A H 0.7461 -0.2154 0.4505 0.101 Uiso 1 1 calc R . . .  
 H14B H 0.8255 -0.1112 0.4336 0.101 Uiso 1 1 calc R . . .  
 H14C H 0.7769 -0.2113 0.3537 0.101 Uiso 1 1 calc R . . .  
 C38 C 0.9071(14) 0.5807(11) 0.3049(11) 0.067(4) Uani 1 1 d . . .  
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N10 N 0.6629(9) 0.4598(8) 0.2728(6) 0.043(3) Uani 1 1 d . . .  
N2 N 0.3459(9) -0.0511(8) 0.3522(7) 0.046(3) Uani 1 1 d . . .  
N9 N 0.5460(10) 0.4714(9) 0.1150(6) 0.048(3) Uani 1 1 d . . .  
N4 N 0.6627(9) 0.1604(8) 0.2770(7) 0.052(3) Uani 1 1 d . . .  
N1 N 0.2090(10) 0.0665(8) 0.3431(6) 0.047(3) Uani 1 1 d . . .  
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N3 N 0.5229(9) 0.0721(7) 0.3958(6) 0.042(3) Uani 1 1 d . . .  
N8 N 0.3529(9) 0.4682(7) 0.1182(6) 0.043(3) Uani 1 1 d . . .  
N5 N 0.0745(12) -0.1737(10) 0.4497(8) 0.061(3) Uani 1 1 d . . .  
N11 N 0.0126(12) 0.3877(9) 0.0100(9) 0.062(3) Uani 1 1 d . . .  
N12 N 0.1728(10) 0.5030(11) 0.2887(8) 0.055(3) Uani 1 1 d . . .  
N6 N 0.0487(15) -0.1688(11) 0.1742(9) 0.074(4) Uani 1 1 d . . .  
O7 O 0.1247(10) 0.4174(8) -0.0032(6) 0.070(3) Uani 1 1 d . . .  
O11 O 0.1673(9) 0.4131(8) 0.2448(6) 0.064(3) Uani 1 1 d . . .  
O8 O -0.0060(8) 0.3729(7) 0.0852(7) 0.063(3) Uani 1 1 d . . .  
O2 O 0.1406(11) -0.2061(10) 0.4015(8) 0.090(4) Uani 1 1 d . . .  
O4 O 0.1609(12) -0.1210(9) 0.1798(7) 0.082(3) Uani 1 1 d . . .  
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O3 O 0.0167(10) -0.2225(9) 0.4999(7) 0.087(3) Uani 1 1 d . . .  
O12 O 0.1683(12) 0.5220(11) 0.3684(7) 0.105(4) Uani 1 1 d . . .  
O5 O 0.0101(9) -0.1815(8) 0.2493(8) 0.081(3) Uani 1 1 d . . .  
O9 O -0.0690(10) 0.3790(9) -0.0433(8) 0.097(4) Uani 1 1 d . . .  
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loop\_

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Cu1 0.0404(10) 0.0672(12) 0.0661(11) 0.0315(9) 0.0038(8) 0.0067(9)  
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C28 0.030(8) 0.061(9) 0.039(7) 0.021(6) 0.008(5) 0.011(7)  
C21 0.057(10) 0.072(10) 0.045(7) 0.013(7) 0.032(7) 0.033(8)  
C6 0.043(9) 0.043(8) 0.042(7) 0.019(6) 0.011(6) 0.012(7)  
C29 0.023(7) 0.054(9) 0.056(8) 0.010(7) 0.005(6) 0.006(7)  
C7 0.043(9) 0.041(7) 0.046(7) 0.016(6) 0.010(6) 0.010(7)  
C16 0.024(8) 0.052(8) 0.062(9) 0.023(7) 0.011(6) 0.011(7)  
C27 0.032(8) 0.057(9) 0.036(7) 0.006(6) 0.007(6) 0.014(7)

C8 0.031(8) 0.056(8) 0.050(7) 0.028(7) 0.011(6) 0.008(7)  
 C2 0.058(11) 0.074(11) 0.058(9) 0.021(8) 0.009(8) 0.034(9)  
 C32 0.028(7) 0.061(9) 0.049(7) 0.019(7) 0.005(6) 0.008(7)  
 C36 0.047(9) 0.050(8) 0.055(8) 0.016(7) 0.021(7) 0.030(7)  
 C10 0.049(9) 0.086(11) 0.035(7) 0.016(7) 0.012(6) 0.040(9)  
 C31 0.049(9) 0.046(8) 0.037(7) 0.008(6) 0.007(6) 0.013(7)  
 C15 0.032(8) 0.064(9) 0.043(7) 0.002(7) 0.005(6) -0.003(7)  
 C1 0.048(9) 0.078(10) 0.041(7) 0.020(7) 0.023(6) 0.037(8)  
 C5 0.057(10) 0.060(9) 0.035(7) 0.010(7) -0.001(6) 0.015(8)  
 C9 0.035(8) 0.078(11) 0.057(8) 0.029(8) -0.001(6) 0.014(7)  
 C30 0.043(9) 0.048(8) 0.052(8) 0.018(7) 0.016(6) 0.007(7)  
 C25 0.042(9) 0.046(8) 0.040(7) 0.005(6) 0.012(6) 0.011(7)  
 C12 0.048(9) 0.039(8) 0.048(7) 0.016(6) 0.003(6) -0.002(6)  
 C35 0.037(8) 0.056(9) 0.052(8) 0.008(7) 0.011(6) 0.018(7)  
 C19 0.048(10) 0.056(10) 0.099(13) 0.041(10) 0.032(9) 0.015(8)  
 C11 0.058(10) 0.048(8) 0.039(7) 0.014(6) 0.002(7) 0.017(8)  
 C26 0.046(9) 0.046(8) 0.041(7) 0.014(6) 0.005(6) 0.017(7)  
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 C39 0.058(11) 0.053(9) 0.063(9) 0.017(8) -0.008(8) 0.017(8)  
 C18 0.041(10) 0.049(9) 0.099(13) 0.021(9) 0.014(9) 0.015(7)  
 C4 0.065(10) 0.057(9) 0.070(9) 0.027(8) -0.003(8) 0.012(8)  
 C22 0.091(14) 0.047(9) 0.077(10) 0.031(8) 0.027(9) 0.025(9)  
 C34 0.055(11) 0.062(10) 0.091(12) 0.019(9) 0.006(9) 0.011(8)  
 C20 0.056(10) 0.073(10) 0.054(8) 0.028(8) 0.023(7) 0.041(9)  
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 C13 0.077(11) 0.082(11) 0.054(8) 0.019(8) 0.014(8) 0.046(9)  
 C3 0.088(13) 0.045(8) 0.056(9) 0.021(7) 0.010(8) 0.018(9)  
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 C24 0.074(11) 0.070(10) 0.066(9) 0.032(8) 0.018(8) 0.039(9)  
 C14 0.058(10) 0.078(11) 0.078(10) 0.023(9) 0.017(8) 0.035(9)  
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O10 0.084(9) 0.072(7) 0.096(8) 0.029(7) 0.022(7) 0.020(6)  
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O6 0.115(11) 0.175(14) 0.072(8) -0.003(8) -0.031(8) 0.071(10)

\_geom\_special\_details

;

All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

;

loop\_

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Cu2 O7 2.010(9) . ?  
Cu2 O8 2.022(9) . ?  
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Cu2 N11 2.396(12) . ?  
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Cu1 N2 1.940(10) . ?  
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Cu1 O2 2.094(12) . ?  
Cu1 O4 2.160(10) . ?  
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Cu1 O1 2.341(14) . ?  
Cu1 N6 2.474(13) . ?  
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loop\_

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loop\_

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'-x, -y, -z'

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_computing_structure_refinement 'SHELXL-97 (Sheldrick, 1997)'
_computing_molecular_graphics 'WingX'
_computing_publication_material 'WingX'

```

```
_refine_special_details
```

```
;
```

Refinement of  $F^2$  against ALL reflections. The weighted R-factor wR and goodness of fit S are based on  $F^2$ , conventional R-factors R are based on F, with F set to zero for negative  $F^2$ . The threshold expression of  $F^2 > 2\text{sigma}(F^2)$  is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-factors based on  $F^2$  are statistically about twice as large as those based on F, and R-factors based on ALL data will be even larger.

```
;
```

```

_refine_ls_structure_factor_coef  Fsqd
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_refine_ls_weighting_scheme      calc
_refine_ls_weighting_details     'calc w=1/[Ws^2^(Fo^2)+(0.0755P)^2+1.3870P] where P=(Fo^2+2Fc^2)/3'
_atom_sites_solution_primary     direct
_atom_sites_solution_secondary   difmap
_atom_sites_solution_hydrogens   geom
_refine_ls_hydrogen_treatment    constr
_refine_ls_extinction_method    none
_refine_ls_extinction_coef      ?
_refine_ls_number_reflns        3911
_refine_ls_number_parameters    217
_refine_ls_number_restraints    0
_refine_ls_R_factor_all         0.0812
_refine_ls_R_factor_gt          0.0478
_refine_ls_wR_factor_ref        0.1836
_refine_ls_wR_factor_gt         0.1547
_refine_ls_goodness_of_fit_ref  1.190
_refine_ls_restrained_S_all     1.190
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_refine_ls_shift/su_mean        0.000

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loop_
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`_atom_site_adp_type`  
`_atom_site_occupancy`  
`_atom_site_symmetry_multiplicity`  
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`_atom_site_refinement_flags`  
`_atom_site_disorder_assembly`  
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Br1 Br 0.47384(8) 0.24642(7) 0.46918(5) 0.0541(2) Uani 1 1 d . . .  
Br2 Br 1.01440(9) 0.76804(9) 0.53266(5) 0.0617(2) Uani 1 1 d . . .  
N1 N 0.6046(5) 0.3855(5) 0.2571(3) 0.0344(9) Uani 1 1 d . . .  
N2 N 0.7211(6) 0.5625(5) -0.0379(4) 0.0411(10) Uani 1 1 d . . .  
N3 N 0.6816(6) 0.6733(5) 0.1054(3) 0.0386(10) Uani 1 1 d . . .  
N4 N 0.8633(5) 0.7161(5) 0.3574(3) 0.0363(9) Uani 1 1 d . . .  
C1 C 0.6064(7) 0.2475(6) 0.3315(4) 0.0402(11) Uani 1 1 d . . .  
C2 C 0.6945(8) 0.1089(7) 0.3158(5) 0.0486(13) Uani 1 1 d . . .  
H2 H 0.6905 0.0156 0.3713 0.058 Uiso 1 1 calc R . .  
C3 C 0.7878(9) 0.1150(7) 0.2150(6) 0.0542(15) Uani 1 1 d . . .  
H3 H 0.8498 0.0249 0.2007 0.065 Uiso 1 1 calc R . .  
C4 C 0.7885(8) 0.2578(7) 0.1345(5) 0.0482(13) Uani 1 1 d . . .  
H4 H 0.8510 0.2643 0.0656 0.058 Uiso 1 1 calc R . .  
C5 C 0.6947(6) 0.3903(6) 0.1582(4) 0.0374(11) Uani 1 1 d . . .  
C6 C 0.6969(6) 0.5420(6) 0.0748(4) 0.0343(10) Uani 1 1 d . . .  
C7 C 0.7243(7) 0.7157(6) -0.0856(4) 0.0384(11) Uani 1 1 d . . .  
C8 C 0.7468(8) 0.8008(8) -0.2013(5) 0.0528(15) Uani 1 1 d . . .  
H8 H 0.7591 0.7566 -0.2610 0.063 Uiso 1 1 calc R . .  
C9 C 0.7501(9) 0.9520(8) -0.2238(6) 0.0614(17) Uani 1 1 d . . .  
H9 H 0.7643 1.0109 -0.3002 0.074 Uiso 1 1 calc R . .  
C10 C 0.7326(9) 1.0194(8) -0.1345(6) 0.0652(18) Uani 1 1 d . . .  
H10 H 0.7366 1.1216 -0.1530 0.078 Uiso 1 1 calc R . .  
C11 C 0.7094(8) 0.9375(7) -0.0192(6) 0.0540(15) Uani 1 1 d . . .  
H11 H 0.6980 0.9818 0.0403 0.065 Uiso 1 1 calc R . .  
C12 C 0.7042(7) 0.7861(6) 0.0021(5) 0.0397(11) Uani 1 1 d . . .  
C13 C 0.6827(6) 0.6906(6) 0.2208(4) 0.0370(11) Uani 1 1 d . . .  
H13A H 0.6294 0.6155 0.2759 0.044 Uiso 1 1 calc R . .  
H13B H 0.6141 0.7921 0.2189 0.044 Uiso 1 1 calc R . .  
C14 C 0.8621(6) 0.6699(5) 0.2626(4) 0.0333(10) Uani 1 1 d . . .  
C15 C 1.0118(7) 0.6075(6) 0.2125(5) 0.0430(12) Uani 1 1 d . . .  
H15 H 1.0074 0.5781 0.1466 0.052 Uiso 1 1 calc R . .  
C16 C 1.1678(7) 0.5894(7) 0.2616(5) 0.0486(13) Uani 1 1 d . . .  
H16 H 1.2700 0.5478 0.2288 0.058 Uiso 1 1 calc R . .  
C17 C 1.1717(7) 0.6332(7) 0.3596(5) 0.0460(13) Uani 1 1 d . . .

H17 H 1.2749 0.6208 0.3955 0.055 Uiso 1 1 calc R . .  
C18 C 1.0163(7) 0.6959(6) 0.4014(4) 0.0404(12) Uani 1 1 d . . .

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\_atom\_site\_aniso\_U\_11  
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Br1 0.0595(4) 0.0588(4) 0.0395(3) -0.0075(3) 0.0090(3) -0.0194(3)  
Br2 0.0590(4) 0.0906(5) 0.0508(4) -0.0387(4) -0.0028(3) -0.0226(4)  
N1 0.033(2) 0.038(2) 0.030(2) -0.0100(16) 0.0024(16) -0.0061(17)  
N2 0.046(3) 0.046(3) 0.034(2) -0.0137(19) 0.0012(18) -0.015(2)  
N3 0.045(2) 0.041(2) 0.031(2) -0.0134(18) 0.0028(18) -0.010(2)  
N4 0.041(2) 0.037(2) 0.033(2) -0.0132(17) 0.0005(17) -0.0096(18)  
C1 0.035(3) 0.046(3) 0.039(3) -0.011(2) -0.001(2) -0.012(2)  
C2 0.055(3) 0.043(3) 0.048(3) -0.010(2) -0.002(3) -0.017(3)  
C3 0.062(4) 0.036(3) 0.066(4) -0.019(3) 0.000(3) -0.010(3)  
C4 0.056(4) 0.047(3) 0.045(3) -0.020(3) 0.008(3) -0.013(3)  
C5 0.036(3) 0.042(3) 0.036(3) -0.015(2) -0.001(2) -0.008(2)  
C6 0.034(2) 0.042(3) 0.029(2) -0.016(2) 0.0005(19) -0.007(2)  
C7 0.035(3) 0.045(3) 0.033(2) -0.009(2) -0.002(2) -0.010(2)  
C8 0.054(4) 0.069(4) 0.032(3) -0.009(3) 0.001(2) -0.018(3)  
C9 0.059(4) 0.066(4) 0.045(3) 0.004(3) 0.000(3) -0.018(3)  
C10 0.062(4) 0.047(4) 0.075(5) -0.001(3) -0.002(3) -0.016(3)  
C11 0.059(4) 0.044(3) 0.058(4) -0.013(3) -0.002(3) -0.013(3)  
C12 0.035(3) 0.041(3) 0.040(3) -0.010(2) -0.002(2) -0.006(2)  
C13 0.039(3) 0.045(3) 0.029(2) -0.021(2) 0.010(2) -0.008(2)  
C14 0.042(3) 0.029(2) 0.029(2) -0.0090(18) 0.003(2) -0.010(2)  
C15 0.048(3) 0.045(3) 0.038(3) -0.021(2) 0.010(2) -0.007(2)  
C16 0.039(3) 0.051(3) 0.056(3) -0.023(3) 0.008(2) -0.007(3)  
C17 0.036(3) 0.051(3) 0.051(3) -0.017(3) 0.001(2) -0.010(2)  
C18 0.050(3) 0.042(3) 0.035(3) -0.014(2) 0.001(2) -0.018(2)

\_geom\_special\_details

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All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

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Br1 C1 1.900(5) . ?  
Br2 C18 1.915(5) . ?  
N1 C1 1.326(6) . ?  
N1 C5 1.340(6) . ?  
N2 C6 1.320(6) . ?  
N2 C7 1.386(7) . ?  
N3 C6 1.378(6) . ?  
N3 C12 1.396(6) . ?  
N3 C13 1.457(6) . ?  
N4 C18 1.323(7) . ?  
N4 C14 1.353(6) . ?  
C1 C2 1.383(8) . ?  
C2 C3 1.371(9) . ?  
C3 C4 1.393(8) . ?  
C4 C5 1.388(8) . ?  
C5 C6 1.473(7) . ?  
C7 C8 1.399(7) . ?  
C7 C12 1.401(8) . ?  
C8 C9 1.376(10) . ?  
C9 C10 1.399(10) . ?  
C10 C11 1.387(9) . ?  
C11 C12 1.384(8) . ?  
C13 C14 1.511(7) . ?  
C14 C15 1.379(7) . ?  
C15 C16 1.377(8) . ?  
C16 C17 1.380(8) . ?  
C17 C18 1.367(8) . ?

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C1 N1 C5 117.0(4) . . ?  
C6 N2 C7 104.9(4) . . ?  
C6 N3 C12 105.5(4) . . ?  
C6 N3 C13 129.3(4) . . ?  
C12 N3 C13 123.7(4) . . ?  
C18 N4 C14 116.4(4) . . ?

N1 C1 C2 125.4(5) . . ?  
N1 C1 Br1 115.5(4) . . ?  
C2 C1 Br1 119.1(4) . . ?  
C3 C2 C1 117.2(5) . . ?  
C2 C3 C4 119.1(6) . . ?  
C5 C4 C3 119.2(5) . . ?  
N1 C5 C4 122.1(5) . . ?  
N1 C5 C6 118.2(4) . . ?  
C4 C5 C6 119.7(5) . . ?  
N2 C6 N3 113.6(4) . . ?  
N2 C6 C5 121.9(4) . . ?  
N3 C6 C5 124.5(4) . . ?  
N2 C7 C8 130.1(5) . . ?  
N2 C7 C12 110.2(4) . . ?  
C8 C7 C12 119.7(5) . . ?  
C9 C8 C7 117.7(6) . . ?  
C8 C9 C10 121.6(6) . . ?  
C11 C10 C9 121.7(6) . . ?  
C12 C11 C10 116.2(6) . . ?  
C11 C12 N3 131.2(5) . . ?  
C11 C12 C7 123.0(5) . . ?  
N3 C12 C7 105.7(5) . . ?  
N3 C13 C14 112.8(4) . . ?  
N4 C14 C15 122.2(5) . . ?  
N4 C14 C13 113.2(4) . . ?  
C15 C14 C13 124.6(4) . . ?  
C16 C15 C14 119.0(5) . . ?  
C15 C16 C17 119.7(5) . . ?  
C18 C17 C16 116.7(5) . . ?  
N4 C18 C17 125.9(5) . . ?  
N4 C18 Br2 115.5(4) . . ?  
C17 C18 Br2 118.5(4) . . ?

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